

## **ROTATABLE RESPONSE SURFACE DESIGNS IN THE PRESENCE OF DIFFERENTIAL NEIGHBOUR EFFECTS FROM ADJOINING EXPERIMENTAL UNITS**

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**ABSTRACT :** In RSM, it is generally assumed that the observations are independent and there is no overlap effects from the neighbouring units. But in situations where the units are placed linearly side by side, there is a chance to have overlap effects/neighbour effects from the adjoining experiments units. For example, in field experiments if a chemical spray is applied to one plot, it may spread over to the nearby plots due to wind. Hence, the response from a particular plot may be affected by effects from the adjacent plots and this effect has to be included in the model while fitting RSM. In this paper, first and second order response surface models with differential effects from adjoining left and right neighbouring units has been considered and the conditions for the model with differential neighbour effects to be rotatable have been obtained. Method of obtaining designs satisfying the derived conditions has been described. An illustration to show the impact of including neighbour effects in the model on the parameter estimates has also been given using a simulated data set. These designs result in more precise estimates of the parameters of the response surface model.

**Keywords and phrases :** Response surface; Differential neighbour effects; Orthogonal estimation; FORDDNE; SORDDNE.

### 1. INTRODUCTION

Response Surface Methodology (RSM) consists of the experimental strategy for exploring relationship between the response variable and the input variables and to develop an appropriate relationship between them. It is used

in situations where several input variables influence some performance measure or quality characteristic of a process. For details on response surface methodology, one can refer to Khuri and Cornell (1996), Montgomery and Peck (2006) and Myers et al. (2009).

The independence of observations cannot be ensured when experimental units are nearby without any separation. For example, in field experiments if a chemical fertilizer is applied to one plot, it may spread over to the nearby plots due to water seepage. Thus the response from a particular plot may also be affected by treatments applied to the adjacent plots and this effect of neighbouring plots has to be included in the model while fitting response surfaces. Hence, it is important to include the neighbour effects in the model to have the proper specification. The interdependence of plots are known in literature by different names viz., interference effects, neighbour effects, indirect effects, competition effect etc.

Indirect effects are effects which occur in an experiment due to the units which are adjacent (spatially or temporally) to the unit being observed. Spatial indirect effects arise due to the treatments applied to the adjacent neighbouring units/ plots and the designs so developed are called Neighbour Balanced Designs (NBDs) whereas temporal indirect effects occur because of the carryover or residual effects in the periods following the periods of their direct application and the designs considering temporal effects are called Crossover Designs. A large number of such designs have been developed in the literature. For details of NBDs, one can refer to Azais et al. (1993), Monod and Bailey (1993), Azais and Druilhet (1997), Azais et al. (1998), Bailey (2003), Bailey and Druilhet (2004), Tomar et al. (2005), Jaggi et al. (2006), Jaggi et al. (2007) and Pateria et al. (2007). For details of crossover designs, one can refer to Williams (1949), Patterson and Lucas (1962), Bal-aam (1968), Sharma (1975), Dey and Balachandran (1976), Sharma (1981), Sharma (1982), Afsarinejad (1990), Varghese and Sharma (2000), Sharma et al. (2002), Sharma et al. (2003) and Bose and Dey (2009). A software for the on line generation of such designs is available (Jaggi et al., 2015). Besides, incorporation of neighbour effects under two-way blocking setup is discussed by several authors [Freeman (1979), Federer and Basford (1991), Chan and Eccleston (2003), Varghese et al. (2011) and Varghese et al. (2014)].

The literature available on response surface designs incorporating neighbour effects is very few. Bartlett (1978) made an attempt to study the neighbouring plot-response relationships. Draper and Guttman (1980) suggested a general linear model for response surface problems in which it is anticipated that the response on a particular unit will be affected by overlap effects from neighbouring units and the same have been illustrated.

Sarika et al. (2008) studied first order response surface model with equal neighbour effects and the conditions were derived for the orthogonal estimation of coefficients of this model and for constancy of the variances of the parameter estimates. Sarika et al. (2009) studied second order response surface model assuming equal neighbour effects and the expressions for the parameters were derived. A method of obtaining designs satisfying the de-

rived conditions was given.

Jaggi et al. (2010) showed that if the neighbour effect is present and is included in the model, there is a substantial reduction in the residual sum of squares and the response is predicted more precisely. Therefore, it can be used to develop an appropriate approximating relationship between the response variable and the input variables when the experimental units are nearby and induce some neighbouring effects.

In response surface studies incorporating neighbour effects, it is unreasonable to expect the equal neighbour effects from adjacent plots always. Hence, we relax this condition of equality of neighbouring effects and present here response surface methodology considering differential effects from adjoining left and right neighbouring units and show that equality of variances as a particular case.

Consider the response surface model:

$$\mathbf{y}_u = f(\mathbf{X}_u) + e_u \quad u = 1, 2, \dots, N,$$

where  $\mathbf{y}_u$  is the response at the point  $u$  with input vector  $\mathbf{X}_u = (X_{1u}, X_{2u}, \dots, X_{vu})'$  of  $v$  components. We consider that the performance of a unit is influenced by the immediate left and immediate right units. Then, the model incorporating the differential neighbour effects from adjoining left and right neighbouring units can be written as:

$$y_{u'} = \sum_{u=1}^N g_{uu'} f(X_u) + e_{u'}, u' = 1, 2, \dots, N \quad (1.1)$$

where

$$\left. \begin{aligned} g_{uu'} &= 1, \text{ if } u = u' \\ &= \alpha_1, |\alpha_1| < 1, \text{ if } u - u' = 1, u' < u \\ &= \alpha_2, |\alpha_2| < 1, \text{ if } u' - u = 1, u' > u \\ &= 0, \text{ otherwise.} \end{aligned} \right\} \quad (1.2)$$

Here,  $\alpha_1$  represents left neighbour effect and  $\alpha_2$  represents the right neighbour effect. The layout of the experiment for estimating this model includes border units for the end units with  $\mathbf{X}$  matrix given below at (2.1) and (3.2).

Direct effects of the border units are ignored. Thus, model (1.1) can be written as

$$\mathbf{Y} = \mathbf{GX}\boldsymbol{\beta} + \mathbf{e}, \quad (1.3)$$

where  $\mathbf{G} = (g_{uu'})$  is the  $N \times (N + 2)$  neighbour matrix. For a first order model,  $\mathbf{X}$  is a  $(N + 2) \times (v + 1)$  matrix of  $N$  points (runs) with two border units and  $v$  predictor variables with first column of unities,  $\boldsymbol{\beta}$  is a  $(v + 1) \times 1$  vector of parameters and  $\mathbf{e}$  is  $N \times 1$  vector of errors which is  $N(\mathbf{0}, \sigma^2 \mathbf{I})$ . If  $\mathbf{G}$  is known, the ordinary least squares (OLS) estimate of  $\boldsymbol{\beta}$ , in the presence of neighbour effects, is :

$$\hat{\boldsymbol{\beta}} = (\mathbf{Z}'\mathbf{Z})^{-1} \mathbf{Z}'\mathbf{Y}, \quad (1.4)$$

where  $\mathbf{Z} = \mathbf{GX}$  with  $D(\hat{\beta}) = \sigma^2(\mathbf{Z}'\mathbf{Z})^{-1}$ .

For example, when  $v = 2$  and  $N = 6$ , then

$$\mathbf{X} = \begin{bmatrix} 1 & x_{16} & x_{26} \\ 1 & x_{11} & x_{21} \\ 1 & x_{12} & x_{22} \\ 1 & x_{13} & x_{23} \\ 1 & x_{14} & x_{24} \\ 1 & x_{15} & x_{25} \\ 1 & x_{16} & x_{26} \\ 1 & x_{11} & x_{21} \end{bmatrix}$$

$$\mathbf{G} = \left[ \begin{array}{c|ccc|ccc|c} \alpha_1 & 1 & \alpha_2 & 0 & 0 & 0 & 0 & 0 \\ 0 & \alpha_1 & 1 & \alpha_2 & 0 & 0 & 0 & 0 \\ 0 & 0 & \alpha_1 & 1 & \alpha_2 & 0 & 0 & 0 \\ 0 & 0 & 0 & \alpha_1 & 1 & \alpha_2 & 0 & 0 \\ 0 & 0 & 0 & 0 & \alpha_1 & 1 & \alpha_2 & 0 \\ 0 & 0 & 0 & 0 & 0 & \alpha_1 & 1 & \alpha_2 \end{array} \right]$$

$$\mathbf{GX} = \mathbf{Z} = \left[ \begin{array}{ccc} (1 + \alpha_1 + \alpha_2) & x_{11} + \alpha_1 x_{16} + \alpha_2 x_{12} & x_{21} + \alpha_1 x_{26} + \alpha_2 x_{22} \\ (1 + \alpha_1 + \alpha_2) & x_{12} + \alpha_1 x_{11} + \alpha_2 x_{13} & x_{22} + \alpha_1 x_{21} + \alpha_2 x_{22} \\ (1 + \alpha_1 + \alpha_2) & x_{13} + \alpha_1 x_{12} + \alpha_2 x_{14} & x_{23} + \alpha_1 x_{22} + \alpha_2 x_{24} \\ (1 + \alpha_1 + \alpha_2) & x_{14} + \alpha_1 x_{13} + \alpha_2 x_{15} & x_{24} + \alpha_1 x_{23} + \alpha_2 x_{25} \\ (1 + \alpha_1 + \alpha_2) & x_{15} + \alpha_1 x_{14} + \alpha_2 x_{16} & x_{25} + \alpha_1 x_{24} + \alpha_2 x_{26} \\ (1 + \alpha_1 + \alpha_2) & x_{16} + \alpha_1 x_{15} + \alpha_2 x_{11} & x_{26} + \alpha_1 x_{25} + \alpha_2 x_{21} \end{array} \right]$$

*Note :* If  $\alpha_1$  and  $\alpha_2$  are known,  $\hat{\beta}_i$ 's are best linear unbiased estimates for  $\beta_i$ 's. However, the values of  $\alpha_1$  and  $\alpha_2$  are hardly known in practice. In that case, one of the procedures, that has been adopted here, is to estimate  $\beta_i$ 's by scanning the entire range of  $\alpha_1, \alpha_2 \in \{0, 1\}$  and choose the values for which the residual sum of squares is minimum. The estimates are still supposed to have their asymptotic properties.

## 2. FIRST ORDER RESPONSE SURFACE MODEL WITH DIFFERENTIAL NEIGHBOUR EFFECTS

Here, the function  $f(x_u)$  takes the form  $f(x_u) = \beta_0 + \sum_{i=1}^v \beta_i x_{iu}$ . The response surface model for  $v = 2$  incorporating indirect effect can be expressed as

$y_u = (1 + \alpha_i + \alpha_2)\beta_0 + \beta_1(x_{1u} + \alpha_1 x_{1,u-1} + \alpha_2 x_{1,u+1}) + \beta_2(x_{2u} + \alpha_1 x_{2,u-1} + \alpha_2 x_{2,u+1}) + \varepsilon_u$ , where  $u = 1, 2, \dots, N$ ,  $u = 0$  for left most border plot and  $u = N + 1$  for right most border plot.

In matrix notation, for  $v$  factors, the  $(N+2) \times (v+1)$  matrix  $\mathbf{X}$  with two extra points as border points is

$$\mathbf{X} = \begin{bmatrix} 1 & x_{1N} & x_{2N} & . & . & . & x_{iN} & . & . & . & x_{vN} \\ 1 & x_{11} & x_{21} & . & . & . & x_{i1} & . & . & . & x_{v1} \\ 1 & x_{12} & x_{22} & . & . & . & x_{i2} & . & . & . & x_{v2} \\ . & . & . & . & . & . & . & . & . & . & . \\ . & . & . & . & . & . & . & . & . & . & . \\ . & . & . & . & . & . & . & . & . & . & . \\ 1 & x_{1u} & x_{2u} & . & . & . & x_{iu} & . & . & . & x_{vu} \\ . & . & . & . & . & . & . & . & . & . & . \\ . & . & . & . & . & . & . & . & . & . & . \\ . & . & . & . & . & . & . & . & . & . & . \\ 1 & x_{1N} & x_{2N} & . & . & . & x_{iN} & . & . & . & x_{vN} \\ 1 & x_{11} & x_{21} & . & . & . & x_{i1} & . & . & . & x_{v1} \end{bmatrix} \quad (2.1)$$

The neighbour matrix  $\mathbf{G}$  is of the form (1.2) which yields  $\mathbf{Z}'\mathbf{Z}$  as:

$$\begin{bmatrix} pN & p \sum_{u=1}^N X_{1u} & p \sum_{u=1}^N X_{2u} & \dots & p \sum_{u=1}^N X_{iu} & \dots & p \sum_{u=1}^N X_{vu} \\ q \sum_{u=1}^N X_{1u}^2 + A_1 & q \sum_{u=1}^N X_{1u} X_{2u} & \dots & q \sum_{u=1}^N X_{1u} X_{iu} + C_{1i} & \dots & q \sum_{u=1}^N X_{1u} X_{vu} + C_{1v} \\ q \sum_{u=1}^N X_{2u}^2 + A_2 & \dots & q \sum_{u=1}^N X_{2u} X_{iu} + C_{2i} & \dots & q \sum_{u=1}^N X_{2u} X_{vu} + C_{2v} \\ . & . & . & . & . & . \\ . & . & . & . & . & . \\ . & . & . & . & . & . \\ q \sum_{u=1}^N X_{1u}^2 + A_i & \dots & q \sum_{u=1}^N X_{iu} X_{vu} + C_{iv} \\ . & . & . & . & . & . \\ . & . & . & . & . & . \\ q \sum_{u=1}^N X_{vu}^2 + A_v \end{bmatrix} \quad (2.2)$$

where  $p = (1 + \alpha_1 + \alpha_2)^2$  and  $q = (1 + \alpha_1^2 + \alpha_2^2)$ , with  $\alpha_1 + \alpha_2 \neq -1$ , otherwise  $|\mathbf{Z}'\mathbf{Z}| = 0$ . Further,

$$A_i = 2\alpha_1\alpha_2 \left[ \sum_{u=1}^N X_{iu} X_{i[(u+2) \bmod N]} \right] + 2(\alpha_1 + \alpha_2) \left[ \sum_{u=1}^N X_{iu} X_{i[(u+1) \bmod N]} \right]$$

$$i = 1, 2, \dots, v;$$

and

$$C_{ii'} = \alpha_1\alpha_2 \left[ \sum_{u=1}^N X_{iu} X_{i'[(u+2) \bmod N]} \right] + \sum_{u=1}^N X_{i[(u+2) \bmod N]} X_{i'u} +$$

$$(\alpha_1 + \alpha_2) \left[ \sum_{u=1}^N X_{iu} X_{i'[(u+1) \bmod N]} + \sum_{u=1}^N X_{iu} X_{i'[(u-1) \bmod N]} \right] \\ \forall i \neq i' = 1, 2, \dots, v.$$

To ensure orthogonality in the estimation of the parameters,  $\mathbf{Z}'\mathbf{Z}$  has to be diagonal. This gives rise to the following conditions:

$$\begin{aligned} \text{i) } \sum_{u=1}^N X_{iu} &= 0 & \forall i = 1, 2, \dots, v; \\ \text{ii) } \sum_{u=1}^N X_{iu} X_{i'u} &= 0 & \forall i \neq i' = 1, 2, \dots, v; \\ \text{iii) } C_{ii'} &= 0 & \forall i \neq i' = 1, 2, \dots, v. \end{aligned} \quad (2.3)$$

After imposing the restrictions, the normal equations for the estimation of  $(v+1)$  parameters are

$$\begin{bmatrix} N(1 + \alpha_1 + \alpha_2)^2 & \mathbf{0}' \\ \mathbf{0} & \mathbf{S} \end{bmatrix} \begin{bmatrix} \beta_0 \\ \boldsymbol{\theta} \end{bmatrix} = \begin{bmatrix} Y. \\ \mathbf{T} \end{bmatrix}, \quad (2.4)$$

where  $\boldsymbol{\theta} = (\beta_1 \beta_2 \dots \beta_v)'$  is the  $v \times 1$  vector of parameters corresponding to predictor variables,  $Y. = \sum_{u=1}^N y_u$  and  $\mathbf{T} = (T_1, T_2, \dots, T_v)'$ ,  $T_i = \sum_{u=1}^N X_{iu} y_u$   $i = 1, 2, \dots, v$  and

$$\mathbf{S} = \text{diag} \left\{ \left[ (1 + \alpha_1^2 + \alpha_2^2) \sum_{u=1}^N X_{1u}^2 + A_1 \right] \dots \right. \\ \left. \left[ (1 + \alpha_1^2 + \alpha_2^2) \sum_{u=1}^N X_{iu}^2 + A_i \right] \dots \left[ (1 + \alpha_1^2 + \alpha_2^2) \sum_{u=1}^N X_{vu}^2 + A_v \right] \right\}$$

Equation (2.4) gives

$$\begin{bmatrix} \hat{\beta}_0 \\ \hat{\boldsymbol{\theta}} \end{bmatrix} = \begin{bmatrix} N^{-1}(1 + \alpha_1 + \alpha_2)^{-2} Y. \\ \mathbf{S}^{-1} \mathbf{T} \end{bmatrix} \quad (2.5)$$

Hence, the variance of parameter estimates is obtained as

$$\begin{aligned} V(\hat{\beta}_0) &= \frac{\sigma^2}{N(1 + \alpha_1 + \alpha_2)^2}; \\ V(\hat{\beta}_i) &= \frac{\sigma^2}{\left[ (1 + \alpha_1^2 + \alpha_2^2) \sum_{u=1}^N X_{iu}^2 + A_i \right]}, \text{ for } i = 1, 2, \dots, v. \end{aligned}$$

The estimated response at a point, say  $\mathbf{x}_0$  is  $\hat{y}_0 = \mathbf{x}_0' \hat{\boldsymbol{\beta}}$  with variance

$$V(\hat{y}_0) = \mathbf{x}'_0 V(\hat{\beta}) \mathbf{x}_0 = \sigma^2 \mathbf{x}'_0 (\mathbf{Z}' \mathbf{Z})^{-1} \mathbf{x}_0$$

Thus,

$$V(\hat{y}_0) = \sigma^2 \left\{ \frac{1}{[N(1+\alpha_1+\alpha_2)^2]} + \frac{x_{10}^2}{\left[ (1+\alpha_1^2+\alpha_2^2) \sum_{u=1}^N X_{1u}^2 + A_1 \right]} + \frac{x_{20}^2}{\left[ (1+\alpha_1^2+\alpha_2^2) \sum_{u=1}^N X_{2u}^2 + A_2 \right]} \right. \\ \left. + \dots + \frac{x_{i0}^2}{\left[ (1+\alpha_1^2+\alpha_2^2) \sum_{u=1}^N X_{1u}^2 + A_i \right]} + \dots + \frac{x_{v0}^2}{\left[ (1+\alpha_1^2+\alpha_2^2) \sum_{u=1}^N X_{vu}^2 + A_v \right]} \right\} \quad (2.6)$$

Now, the following restrictions are imposed to ensure the constancy of the variances of the parameter estimates

$$\begin{aligned} \text{i) } & \sum_{u=1}^N X_{iu}^2 = \delta, \text{ a constant } \forall i = 1, 2, \dots, v \\ \text{ii) } & A_i = A, \text{ a constant } \forall i \neq i' = 1, 2, \dots, v \end{aligned} \quad (2.7)$$

Therefore,

$$V(\hat{y}_0) = \sigma^2 \left\{ \frac{1}{N(1+\alpha_1+\alpha_2)^2} + \frac{\sum_{u=1}^N X_{i0}^2}{(1+\alpha_1^2+\alpha_2^2)\delta + A} \right\}$$

Hence, the variances of  $\hat{\beta}_i$ 's ( $i = 1, 2, \dots, v$ ) are same and it is seen that the variance of estimated response is a function of  $\sum_{i=1}^v X_{i0}^2$ . For given  $\alpha_1$  and  $\alpha_2$ ,

the points for which  $\sum_{i=1}^v X_{i0}^2$  is same, the estimated response will have the same variance. The designs satisfying this property are called First Order Rotatable Designs with Differential Neighbour Effects (FORDDNE).

**Remark 2.1** For  $\alpha_1 = \alpha_2 = \alpha$ , the above expressions reduce to those given in Sarika *et al.* (2008).

## 2.1 Method of Constructing FORDDNE

Construct a  $2^v$  full factorial in lexicographic order with levels  $(-1, 1)$  giving a rectangle  $R$  of  $2^v$  rows and  $v$  columns with entries  $-1$  and  $1$ . Circular rotation

of the columns of  $R$ ,  $(v - 1)$  times, yields  $(v - 1)$  sets each consisting of  $2^v$  rows and  $v$  columns. By appending these sets below  $R$  one after another, we obtain a rectangular array of  $v \times 2^v$  rows and  $v$  columns. Appending another column of unity resulting in  $(v + 1)$  columns, a FORDDNE in  $v \times 2^v$  points is obtained by adding two extra points of border units such that each end of the array has a point of the other end.

**Example 2.1** Let  $v = 3$ . The  $24 \times 4$  of a FORDDNE developed from a complete  $2^3$  factorial with levels  $-1$  and  $1$  by rotating its columns 2 times with first column of 1's, the coefficient of mean, and two extra points as border points is written as follows:



$$\begin{bmatrix} 1 & -1 & -1 & -1 \\ 1 & 1 & 1 & 1 \\ 1 & 1 & 1 & -1 \\ 1 & 1 & -1 & 1 \\ 1 & 1 & -1 & -1 \\ 1 & -1 & 1 & 1 \\ 1 & -1 & 1 & -1 \\ 1 & -1 & -1 & 1 \\ 1 & -1 & -1 & -1 \\ 1 & 1 & 1 & 1 \\ 1 & -1 & 1 & 1 \\ 1 & 1 & 1 & -1 \\ 1 & -1 & 1 & -1 \\ 1 & 1 & -1 & 1 \\ 1 & -1 & -1 & 1 \\ 1 & 1 & -1 & -1 \\ 1 & -1 & -1 & -1 \\ 1 & 1 & 1 & 1 \\ 1 & 1 & -1 & 1 \\ 1 & -1 & 1 & 1 \\ 1 & -1 & -1 & 1 \\ 1 & 1 & 1 & -1 \\ 1 & 1 & -1 & -1 \\ 1 & -1 & 1 & -1 \\ 1 & -1 & -1 & -1 \\ 1 & 1 & 1 & 1 \end{bmatrix}$$

The matrix  $\mathbf{G}$  of order  $27 \times 29$  is of the form given in (1.2). Further.

$$\mathbf{Z}'\mathbf{Z} = \begin{bmatrix} 24(1 + \alpha_1 + \alpha_2)^2 & \mathbf{0}'_{1 \times 3} \\ \mathbf{0}_{3 \times 1} & [4(1 + \alpha_1 + \alpha_2)^2 + 8(1 - \alpha_1 - \alpha_2)^2 + 12]\mathbf{I}_3 \end{bmatrix},$$

with  $\alpha_1 = \alpha_2 \neq -0.5$

Thus,

$$V(\hat{\beta}_0) = \frac{\sigma^2}{24(1 + \alpha_1 + \alpha_2)^2},$$

$$V(\hat{\beta}_i) = \frac{\sigma^2}{[4(1 + \alpha_1 + \alpha_2) + 8(1 - \alpha_1 - \alpha_2)^2 + 12]}, i = 1, 2, 3$$

$$V(\hat{y}_0) = \sigma^2 \left\{ \frac{1}{24(1 + \alpha_1 + \alpha_2)^2} + \frac{3}{12(\alpha_1 + \alpha_2)^2 - 8(1 - \alpha_1 - \alpha_2)^2 + 24} \right\}$$

For  $\alpha_1 = 0.2$  and  $\alpha_2 = 0.4$ ,

$$V(\hat{\beta}_0) = 0.0163\sigma^2, V(\hat{\beta}_i) = 0.0425\sigma^2, i = 1, 2, 3 \text{ and } V(\hat{y}_0) = 0.1438\sigma^2$$

## 2.2 Illustration

For the design given in Example 2.1, following is the synthetic data with plot numbers and treatment combinations:

Border plot (1-1-1-1)	Plot 1 (1111) 144.06	Plot 2 (111-1) 158.62	Plot 3 (11-11) 164.87	Plot 4 (11-1-1) 162.01	Plot 5 (1-111) 131.16
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Plot 6 (1-11-1) 116.94	Plot 7 (1-1-11) 123.25	Plot 8 (1-1-1-1) 137.26	Plot 9 (1111) 140.68	Plot 10 (1-111) 141.06	Plot 11 (111-1) 125.73	Plot 12 (1-11-1) 131.61
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Plot 13 (11-11) 146.75	Plot 14 (11-1-1) 161.87	Plot 15 (1-1-11) 146.77	Plot 16 (11-1-1) 143.93	Plot 17 (1111) 153.43	Plot 18 (11-11) 164.85	Plot 19 (1-111) 148.95
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Plot 20 (1-1-11) 135.75	Plot 21 (111-1) 146.41	Plot 22 (11-11-1) 141.25	Plot 23 (11-1-1) 125.13	Plot 24 (1-1-1-1) 122.35	Border plot (1111)
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Here, plot 1 has border plot as left neighbouring plot and plot 2 as right neighbouring plot, plot 2 has plot 1 as left neighbouring plot and plot 3 as right neighbouring plot and so on. First order response surface model was fitted to these data with three factors. The coefficient of determination ( $R^2$ ), Residual Sum of Squares (RSS) and the parameter estimates for different values of  $\alpha_1$  and  $\alpha_2$  were calculated and are given in Table 2.1. It can be seen that RSS is 2556.45 at  $\alpha_1 = 0$  and  $\alpha_2 = 0$  which decreases as the value of  $\alpha_1$  and  $\alpha_2$  increases and is minimum at  $\alpha_1 = 0.78$  and  $\alpha_2 = 0.47$ . Similar trend can be seen for  $R^2 = 99.98\%$  at  $\alpha_1 = 0.78$  and  $\alpha_2 = 0.47$ . All the parameters except  $\beta_0$  and  $\beta_1$  are not significant at  $\alpha_1 = \alpha_2 = 0$  where as all the parameters become significant at  $\alpha_1 = 0.78$  and  $\alpha_2 = 0.47$  clearly indicating the impact of the neighbouring units. The fitted model at  $\hat{\alpha}_1 = 0.78$  and  $\hat{\alpha}_2 = 0.47$  is:

$$\hat{y} = 63.24 + 9.26X_1 - 4.63X_2 + 5.25X_3$$

The variance of the estimated responses is same for all the points within the design and is obtained as 0.097 at  $\alpha_1 = 0.78$  and  $\alpha_2 = 0.47$ . Hence the design is rotatable. The maximum response corresponds to the maximum dose of the input factors  $X_1$  and  $X_3$  and minimum dose of the input factor  $X_2$ . The variance of the estimated response for all the points within the design at  $\alpha_1 = \alpha_2 = 0$  is worked out as 0.170.

Table 2.1 Results of fitting first order model for  $v = 3$  at different values of  $\alpha_1$  and  $\alpha_2$ 

$\alpha_2$	$\alpha_1$	<b>0.00</b>	<b>0.20</b>	<b>0.40</b>	<b>0.60</b>	<b>0.70</b>	<b>0.75</b>	<b>0.78</b>	<b>0.80</b>	<b>0.90</b>
<b>0.00</b>	$R^2$	0.4480	0.6046	0.7379	0.8172	0.8364	0.8417	0.8436	0.8444	0.8433
	$RSS$	2556.45	1807.39	1198.26	835.79	747.84	723.86	715.13	711.49	716.24
	$\beta_0$	142.28* (2.31)	118.56* (1.62)	101.63* (1.13)	88.92* (0.82)	83.69* (0.73)	81.30* (0.70)	79.93* (0.69)	79.04* (0.68)	74.88* (0.64)
	$\beta_1$	7.34* (2.31)	8.71* (1.97)	9.36* (1.56)	9.26*2 (0.23)	8.99* (1.11)	8.83* (1.07)	8.72* (1.05)	8.64* (1.04)	8.24* (0.99)
	$\beta_2$	-3.63 (2.31)	-4.32 (1.97)	-4.65* (1.56)	-4.61* (1.23)	-4.48* (1.11)	-4.40* (1.07)	-4.35* (1.05)	-4.31* (1.04)	-4.11* (0.99)
	$\beta_3$	4.11 (2.31)	4.89 (1.97)	5.27* (1.56)	5.22* (1.23)	5.08* (1.11)	4.98* (1.07)	4.92* (1.05)	4.88* (1.04)	4.65* (0.99)
<b>0.20</b>	$R^2$	0.5264	0.7086	0.8506	0.9279	0.9432	0.9460	0.9464	0.9461	0.9392
	$RSS$	2165.03	1332.10	683.10	329.50	259.52	246.73	245.22	246.57	277.73
	$\beta_0$	118.57* (1.77)	101.63* (1.19)	88.92* (0.75)	79.04* (0.46)	74.88* (0.39)	72.96* (0.37)	71.86* (0.36)	71.14* (0.36)	67.75* (0.36)
	$\beta_1$	8.12* (2.15)	9.55* (1.71)	10.17* (1.19)	9.97*2 (0.78)	9.65* (0.66)	9.45* (0.63)	9.32* (0.62)	9.23* (0.62)	8.77* (0.62)
	$\beta_2$	-4.03 (2.15)	-4.74* (1.71)	-5.06* (1.19)	-4.97* (0.78)	-4.81* (0.66)	-4.71* (0.63)	-4.65* (0.62)	-4.61* (0.62)	-4.38* (0.62)
	$\beta_3$	4.57 (2.15)	5.38 (1.71)	5.74* (1.19)	5.64* (0.78)	5.46* (0.66)	4.35* (0.63)	5.27* (0.62)	5.23* (0.62)	4.96* (0.62)
<b>0.40</b>	$R^2$	0.5740	0.7585	0.9009	0.9782	0.9932	0.9958	0.9960	0.9956	0.9881
	$RSS$	1947.32	1104.03	452.94	99.82	30.97	19.07	18.22	20.06	54.35
	$\beta_0$	101.63* (1.44)	88.92* (0.89)	79.04* (0.54)	71.14* (0.23)	67.75* (0.12)	66.18* (0.09)	65.27* (0.13)	64.67* (0.09)	61.86* (0.14)
	$\beta_1$	8.25* (1.99)	9.60* (1.47)	10.19* (0.95)	10.00* (0.42)	9.69* (0.22)	9.50* (0.17)	9.37* (0.23)	9.29* (0.17)	8.83* (0.27)
	$\beta_2$	-4.10 (1.99)	-4.78* (1.47)	-5.08* (0.95)	-4.99* (0.42)	-4.84* (0.22)	-4.74* (0.17)	-4.68* (0.23)	-4.64* (0.17)	-4.41* (0.27)
	$\beta_3$	4.65 (1.99)	5.43* (1.47)	5.77* (0.95)	5.66* (0.42)	5.49* (0.22)	5.38* (0.17)	5.31* (0.23)	5.26* (0.17)	5.01* (0.27)
<b>0.45</b>	$R^2$	0.5790	0.7616	0.9029	0.9805	0.9961	0.9991	0.9994	0.9992	0.9923
	$RSS$	1924.50	1089.52	443.76	89.08	17.70	4.32	2.56	3.79	35.01
	$\beta_0$	98.12* (1.38)	86.23* (0.91)	76.91* (0.52)	69.40* (0.21)	66.18* (0.09)	64.67* (0.04)	63.80* (0.03)	63.24* (0.03)	60.54* (0.11)
	$\beta_1$	8.18* (1.95)	9.50* (1.49)	10.08* (0.93)	9.90* (0.39)	9.61* (0.17)	9.42* (0.08)	9.30* (0.06)	9.22* (0.07)	8.77* (0.22)
	$\beta_2$	-4.06 (1.95)	-4.73* (1.49)	-5.02* (0.93)	-4.94* (0.39)	-4.80* (0.17)	-4.70* (0.08)	-4.65* (0.06)	-4.60* (0.07)	-4.38* (0.22)
	$\beta_3$	4.62 (1.95)	5.37* (1.49)	5.71* (0.93)	5.61* (0.39)	5.45* (0.17)	5.34* (0.08)	5.27* (0.06)	5.23* (0.07)	4.98* (0.22)

<b>0.47</b>	$R^2$	0.5803	0.7618	0.9026	0.9804	0.9963	0.9994	0.9998	0.9997	0.9932
	$RSS$	1918.77	1088.76	445.12	89.69	17.04	2.92	0.69	1.59	31.22
	$\hat{\beta}_0$	96.79* (1.36)	85.20* (0.90)	76.08* (0.51)	68.73* (0.21)	65.57* (0.09)	64.09* (0.04)	63.24* (0.02)	62.68* (0.03)	60.03* (0.11)
	$\hat{\beta}_1$	8.14* (1.93)	9.45* (1.48)	10.02* (0.92)	9.86* (0.39)	9.56* (0.16)	9.38* (0.07)	9.26* (0.03)	9.18* (0.03)	8.74* (0.20)
	$\hat{\beta}_2$	-4.05 (1.93)	-4.70* (1.48)	-4.99* (0.92)	-4.92* (0.39)	-4.78* (0.16)	-4.69* (0.07)	-4.63* (0.03)	-4.59* (0.05)	-4.37* (0.20)
<b>0.50</b>	$\hat{\beta}_3$	4.60 (1.93)	5.34* (1.48)	5.68* (0.92)	5.59* (0.39)	5.42* (0.16)	5.32* (0.07)	5.25* (0.03)	5.21* (0.05)	4.96* (0.20)
	$R^2$	0.5814	0.7612	0.9011	0.9791	0.9954	0.9988	0.9994	0.9994	0.9935
	$RSS$	1913.67	1091.58	452.26	95.61	20.84	5.44	2.40	2.77	29.63
	$\hat{\beta}_0$	94.85* (1.33)	83.69* (0.89)	74.88* (0.51)	67.75* (0.21)	64.67* (0.09)	63.24* (0.05)	62.40* (0.03)	61.86* (0.03)	59.28* (0.10)
	$\hat{\beta}_1$	8.08* (1.92)	9.35* (1.47)	9.93* (0.92)	9.77* (0.40)	9.49* (0.18)	9.31* (0.09)	9.20* (0.06)	9.12* (0.06)	8.69* (0.20)
<b>0.60</b>	$\hat{\beta}_2$	-4.01 (1.92)	-4.66* (1.47)	-4.95* (0.92)	-4.88* (0.40)	-4.74* (0.18)	-4.65* (0.09)	-4.60* (0.06)	-4.56* (0.06)	-4.34* (0.20)
	$\hat{\beta}_3$	4.57 (1.92)	5.29* (1.47)	5.62* (0.92)	5.54* (0.40)	5.38* (0.18)	5.28* (0.09)	5.22* (0.06)	5.17* (0.06)	4.93* (0.20)
	$R^2$	0.5791	0.7514	0.8871	0.9661	0.9843	0.9889	0.9903	0.9907	0.9874
	$RSS$	1924.40	1136.56	515.90	154.98	71.56	50.88	44.49	42.55	57.59
	$\hat{\beta}_0$	88.92* (1.25)	79.04* (0.85)	71.14* (0.52)	64.67* (0.26)	61.86* (0.17)	60.54* (0.14)	59.78* (0.13)	59.28* (0.12)	56.91* (0.14)
<b>0.80</b>	$\hat{\beta}_1$	7.79* (1.86)	8.97* (1.45)	9.52* (0.95)	9.42* (0.49)	9.18* (0.32)	9.02* (0.27)	8.92* (0.23)	8.85* (0.24)	8.46* (0.27)
	$\hat{\beta}_2$	-3.87 (1.86)	-4.47* (1.45)	-4.75* (0.95)	-4.70* (0.49)	-4.58* (0.32)	-4.51* (0.27)	-4.46* (0.23)	-4.42* (0.24)	-4.23* (0.27)
	$\hat{\beta}_3$	4.41 (1.86)	5.08* (1.45)	5.40* (0.95)	5.35* (0.49)	5.21* (0.32)	5.12* (0.27)	5.06* (0.23)	5.02* (0.24)	4.81* (0.27)
	$R^2$	0.5530	0.7055	0.8299	0.9099	0.9323	0.9396	0.9428	0.9445	0.9477
	$RSS$	2043.54	1346.50	777.43	412.05	309.27	276.08	261.51	253.91	238.91
<b>0.90</b>	$\hat{\beta}_0$	79.04* (1.47)	71.14* (0.84)	64.67* (0.58)	59.28* (0.39)	56.91* (0.32)	55.80* (0.30)	55.15* (0.29)	54.72* (0.28)	52.70* (0.26)
	$\hat{\beta}_1$	6.98* (1.76)	7.97* (1.44)	8.47* (1.08)	8.48* (0.75)	8.32* (0.63)	8.21* (0.58)	8.14* (0.56)	8.09* (0.55)	7.80* (0.51)
	$\hat{\beta}_2$	-3.48 (1.76)	-3.97* (1.44)	-4.23* (1.08)	-4.24* (0.75)	-4.16* (0.63)	-4.11* (0.58)	-4.07* (0.56)	-4.05* (0.55)	-3.90* (0.51)
	$\hat{\beta}_3$	3.97 (1.76)	4.53 (1.44)	4.82* (1.08)	4.82* (0.75)	4.73* (0.63)	4.67* (0.58)	4.63* (0.56)	4.60* (0.55)	4.44* (0.51)
	$R^2$	0.5333	0.6750	0.7930	0.8725	0.8968	0.9054	0.9094	0.9117	0.9183
<b>0.90</b>	$RSS$	2133.42	1485.71	946.48	582.84	471.74	432.69	414.20	403.82	373.64
	$\hat{\beta}_0$	74.88* (1.11)	67.75* (0.84)	61.86* (0.61)	56.91* (0.44)	54.72* (0.38)	53.69* (0.36)	53.10* (0.35)	52.70* (0.34)	50.82* (0.32)
	$\hat{\beta}_1$	6.54* (1.72)	7.43* (1.44)	7.90* (1.13)	7.96* (0.85)	7.84* (0.75)	7.75* (0.70)	7.69* (0.68)	7.65* (0.67)	7.42* (0.62)
	$\hat{\beta}_2$	-3.26 (1.72)	-3.71* (1.44)	-3.95* (1.13)	-3.98* (0.85)	-3.92* (0.75)	-3.88* (0.70)	-3.85* (0.68)	-3.83* (0.67)	-3.71* (0.62)
	$\hat{\beta}_3$	3.72 (1.72)	4.22 (1.44)	4.50* (1.13)	4.53* (0.85)	4.46* (0.75)	4.41* (0.70)	4.38* (0.68)	4.36* (0.67)	4.22* (0.62)

Figures within parentheses are the standard errors of the estimates  $*p < 0.01$

Even though the method explained above gives designs which ensure the constancy in variance of the estimated response, the number of runs required to layout the experiment is large. This problem of large runs can be solved by considering fractional replication.

**Example 2.2** Consider a  $2^{4-1}$  factorial with four columns for four factors in 8 runs. Rotate the columns cyclically 3 times to obtain 32 points. Finally, add the first run at the bottom and last run at the top as border rows. The  $32 \times 5$  matrix  $\mathbf{X}$  of 4 predictor variables with first column of 1's, the coefficients of mean and two extra points as border points is obtained.

1	1	1	-1	1
1	-1	-1	-1	-1
1	-1	-1	1	1
1	-1	-1	-1	1
1	-1	1	1	-1
1	1	-1	-1	-1
1	1	-1	1	1
1	1	1	-1	1
1	1	1	1	-1

1	-1	-1	-1	-1
1	1	-1	-1	1
1	1	-1	1	-1
1	-1	-1	1	1
1	-1	1	-1	-1
1	1	1	-1	1
1	1	1	1	-1
1	-1	1	1	1

  

1	-1	-1	-1	-1
1	1	1	-1	-1
1	-1	1	-1	1
1	1	-1	-1	1
1	-1	-1	1	-1
1	1	1	1	-1
1	-1	1	1	1
1	1	-1	1	1

1	-1	-1	-1	-1
1	-1	1	1	-1
1	1	-1	1	-1
1	1	1	-1	-1
1	-1	-1	-1	1
1	-1	1	1	1
1	1	-1	1	1
1	1	1	-1	1
1	-1	-1	-1	-1

The variance of the parameter estimates and variance of the estimated response is obtained as  $V(\hat{\beta}_0) = 0.0122\sigma^2$ ,  $V(\hat{\beta}_i) = 0.0309\sigma^2$ , and  $V(\hat{y}_0) = 0.1360\sigma^2$ . The values in the case of full factorial are  $V(\hat{\beta}_0) = 0.0061\sigma^2$ ,  $V(\hat{\beta}_i) = 0.0121\sigma^2$  and  $V(\hat{y}_0) = 0.504\sigma^2$ .

### 3. SECOND ORDER RESPONSE SURFACE MODEL WITH DIFFERENTIAL NEIGHBOUR EFFECTS

We consider the following form of  $f(X_u)$ :

$$f(X_u) = \beta_0 + \sum_{i=1}^v \beta_i X_{iu} + \sum_{i=1}^v \beta_{ii} X_{iu}^2 \quad (3.1)$$

$$\mathbf{X}_{(N+2) \times 5} = \begin{bmatrix} 1 & X_{1N} & X_{2N} & X_{1N}^2 & X_{2N}^2 \\ 1 & X_{11} & X_{21} & X_{11}^2 & X_{21}^2 \\ 1 & X_{12} & X_{22} & X_{12}^2 & X_{22}^2 \\ \vdots & & & & \\ \vdots & & & & \\ 1 & X_{1u} & X_{2u} & X_{1u}^2 & X_{2u}^2 \\ \vdots & & & & \\ \vdots & & & & \\ \vdots & & & & \\ 1 & X_{1N} & X_{2N} & X_{1N}^2 & X_{2N}^2 \\ 1 & X_{11} & X_{21} & X_{11}^2 & X_{21}^2 \end{bmatrix} \quad (3.2)$$

Thus,

$\mathbf{Z}'\mathbf{Z}$  is

$$\begin{bmatrix} pN & p \sum_{u=1}^N X_{1u} & p \sum_{u=1}^N X_{2u} & p \sum_{u=1}^N X_{1u}^2 & p \sum_{u=1}^N X_{2u}^2 \\ q \sum_{u=1}^N X_{1u}^2 + A_1 & q \sum_{u=1}^N X_{1u} X_{2u} + C_1 & q \sum_{u=1}^N X_{1u}^3 + C_2 & q \sum_{u=1}^N X_{1u} X_{2u}^2 + C_3 \\ & q \sum_{u=1}^N X_{2u}^2 + A_2 & q \sum_{u=1}^N X_{1u}^2 + C_4 & q \sum_{u=1}^N X_{2u}^3 + C_5 \\ & & q \sum_{u=1}^N X_{2u}^4 + B_1 & q \sum_{u=1}^N X_{1u}^2 X_{2u}^2 + D \\ & & & q \sum_{u=1}^N X_{2u}^4 + B_2 \end{bmatrix}$$

where  $p = (1 + \alpha_1 + \alpha_2)^2$  and  $q = (1 + \alpha_1^2 + \alpha_2^2)$

where,

$$A_1 = 2\alpha_1\alpha_2 \left[ \sum_{u=1}^N X_{1u}X_{1[(u+2) \bmod N]} \right] + 2(\alpha_1 + \alpha_2) \left[ \sum_{u=1}^N X_{1u}X_{1[(u+1) \bmod N]} \right]$$

$$A_2 = 2\alpha_1\alpha_2 \left[ \sum_{u=1}^N X_{2u}X_{2[(u+2) \bmod N]} \right] + 2(\alpha_1 + \alpha_2) \left[ \sum_{u=1}^N X_{2u}X_{2[(u+1) \bmod N]} \right]$$

$$B_1 = 2\alpha_1\alpha_2 \left[ \sum_{u=1}^N X_{1u}^2 X_{1[(u+2) \bmod N]}^2 \right] + 2(\alpha_1 + \alpha_2) \left[ \sum_{u=1}^N X_{1u}^2 X_{1[(u+1) \bmod N]}^2 \right]$$

$$B_2 = 2\alpha_1\alpha_2 \left[ \sum_{u=1}^N X_{2u}^2 X_{2[(u+2) \bmod N]}^2 \right] + 2(\alpha_1 + \alpha_2) \left[ \sum_{u=1}^N X_{2u}^2 X_{2[(u+1) \bmod N]}^2 \right]$$

$$C_1 = \alpha_1\alpha_2 \left[ \sum_{u=1}^N X_{1u}X_{2[(u+2) \bmod N]} \right] + \left[ \sum_{u=1}^N X_{1[(u+2) \bmod N]}X_{2u} \right] \\ + (\alpha_1 + \alpha_2) \left[ \sum_{u=1}^N X_{1u}X_{1[(u+1) \bmod N]}^2 + \sum_{u=1}^N X_{1u}^2 X_{1[(u+1) \bmod N]}X_{2u} \right]$$

$$C_2 = \alpha_1\alpha_2 \left[ \sum_{u=1}^N X_{1u}X_{1[(u+2) \bmod N]}^2 + \sum_{u=1}^N X_{1u}^2 X_{1[(u+2) \bmod N]} \right] \\ + (\alpha_1 + \alpha_2) \left[ \sum_{u=1}^N X_{1u}X_{1[(u+1) \bmod N]}^2 + \sum_{u=1}^N X_{1u}^2 X_{1[(u+1) \bmod N]}X_{2u} \right]$$

$$C_3 = \alpha_1\alpha_2 \left[ \sum_{u=1}^N X_{1u}X_{2[(u+2) \bmod N]}^2 + \sum_{u=1}^N X_{1[(u+2) \bmod N]}X_{2u}^2 \right] \\ + (\alpha_1 + \alpha_2) \left[ \sum_{u=1}^N X_{1u}X_{2[(u+1) \bmod N]}^2 + \sum_{u=1}^N X_{1[(u+1) \bmod N]}X_{2u}^2 \right]$$

$$C_4 = \alpha_1\alpha_2 \left[ \sum_{u=1}^N X_{1[(u+2) \bmod N]}^2 X_{2u} + \sum_{u=1}^N X_{1u}^2 X_{2[(u+2) \bmod N]} \right] \\ + (\alpha_1 + \alpha_2) \left[ \sum_{u=1}^N X_{1[(u+1) \bmod N]}^2 X_{2u} + \sum_{u=1}^N X_{1u}^2 X_{2[(u+1) \bmod N]} \right]$$

$$\begin{aligned}
C_5 &= \alpha_1 \alpha_2 \left[ \sum_{u=1}^N X_{2u} X_{[(u+2) \bmod N]}^2 + \sum_{u=1}^N X_{2u}^2 X_{2[(u+2) \bmod N]}^2 \right] \\
&\quad + (\alpha_1 + \alpha_2) \left[ \sum_{u=1}^N X_{2u} X_{2[(u+1) \bmod N]}^2 + \sum_{u=1}^N X_{2u}^2 X_{2[(u+1) \bmod N]}^2 \right] \\
D &= \alpha_1 \alpha_2 \left[ \sum_{u=1}^N X_{1u}^2 X_{2[(u+2) \bmod N]}^2 + \sum_{u=1}^N X_{1[(u+2) \bmod N]}^2 X_{2u}^2 \right] \\
&\quad + (\alpha_1 + \alpha_2) \left[ \sum_{u=1}^N X_{1u}^2 X_{2[(u+1) \bmod N]}^2 + \sum_{u=1}^N X_{1[(u+1) \bmod N]}^2 X_{2u}^2 \right]
\end{aligned}$$

For near-orthogonal estimation of parameters and constancy of variances of linear parameters and quadratic parameters, the following conditions are required:

$$\text{i) } \sum_{u=1}^N \prod_{i=1}^2 X_{iu}^{\omega_i} = 0 \text{ for } \omega_i = 0, 1 \text{ or } 3 \text{ and } 0 < \sum \omega_i < 4$$

$$\text{ii) } \sum_{u=1}^N X_{iu}^2 = 0 \text{ constant } N\eta = \delta, \quad \forall i = 1, 2$$

$$\text{iii) } \sum_{u=1}^N X_{iu}^2 X_{i'u}^2 = \text{constant} = N\gamma = L$$

$$\text{iv) } \sum_{u=1}^N X_{iu}^4 = \text{constant} = CL$$

$$\text{v) } A_i = A \text{ and } B_i = B \quad \forall i = 1, 2. \quad (3.3)$$

Therefore,

$$\mathbf{Z}'\mathbf{Z} = \left[ \begin{array}{cc|c} N(1 + \alpha_1 + \alpha_2)^2 & \mathbf{0}'_{1 \times 2} & (1 + \alpha_1 + \alpha_2)^2 \delta \mathbf{1}'_{1 \times 2} \\ \hline \mathbf{0}'_{2 \times 1} & [(1 + \alpha_1^2 + \alpha_2^2)\delta + A]\mathbf{I}_2 & \mathbf{0}_{2 \times 2} \\ \hline (1 + \alpha_1 + \alpha_2)^2 \delta \mathbf{1}_{2 \times 1} & \mathbf{0}_{2 \times 2} & \mathbf{H}_{2 \times 2} \end{array} \right]$$



Thus,

$$(\mathbf{Z}'\mathbf{Z})^{-1} = \begin{bmatrix} \frac{1}{N(1+\alpha_1+\alpha_2)^2} + 2\frac{\delta}{N}\xi & \mathbf{0}'_{1 \times 2} & -\xi\mathbf{1}'_{1 \times 2} \\ \mathbf{0}_{2 \times 1} & \frac{1}{[(1+\alpha_1^2+\alpha_2^2)\delta+A]}\mathbf{I}_2 & \mathbf{0}_{2 \times 2} \\ -\xi\mathbf{1}_{2 \times 1} & \mathbf{0}_{2 \times 2} & \mathbf{\Psi}_{2 \times 2} \end{bmatrix},$$

where,

$$\xi = \frac{\delta}{N} \left[ \frac{[(1+\alpha_1^2+\alpha_2^2)L(C-1)+B-D] + [(1+\alpha_1^2+\alpha_2^2)L+D-\frac{\delta^2}{N}(1+\alpha_1+\alpha_2)^2]}{\Delta} \right],$$

$$\mathbf{\Psi} = \left[ \frac{(1+\alpha_1^2+\alpha_2^2)L(C+1)+B+D-2(1+\alpha_1^2+\alpha_2^2)\frac{\delta^2}{N}}{\Delta} \right] \mathbf{I}_2 \\ + \left[ -\frac{(1+\alpha_1^2+\alpha_2^2)L+D-\frac{\delta^2}{N}(1+\alpha_1+\alpha_2)^2}{\Delta} \right] \mathbf{1}\mathbf{1}'$$

and

$$\Delta = [(1+\alpha_1^2+\alpha_2^2)L(C-1)+B-D]\{[(1+\alpha_1^2+\alpha_2^2)L(C-1)+B-D] \\ + 2[(1+\alpha_1^2+\alpha_2^2)L+D-\frac{\delta^2}{N}(1+\alpha_1+\alpha_2)^2]\}$$

The variances of the parameter estimates and covariances between the parameter estimates are obtained as

$$V(\hat{\beta}_0) = \frac{\sigma^2}{N(1+\alpha_1+\alpha_2)^2} [1+2\delta(1+\alpha_1+\alpha_2)^2\xi] \\ V(\hat{\beta}_i) = \frac{\sigma^2}{[(1+\alpha_1^2+\alpha_2^2)\delta+A]}, i = 1, 2 \quad (3.4)$$

$$V(\hat{\beta}_{ii}) = \sigma^2 \frac{(1+\alpha_1^2+\alpha_2^2)L(C+1)+B+D-2(1+\alpha_1^2+\alpha_2^2)\frac{\delta^2}{N}}{\Delta}$$

$$\text{Cov}(\hat{\beta}_0, \hat{\beta}_{ii}) = -\sigma^2\xi$$

$$\text{Cov}(\hat{\beta}_{ii}, \hat{\beta}_{i'i'}) = -\sigma^2 \left[ -\frac{(1+\alpha_1^2+\alpha_2^2)L+D-\frac{\delta^2}{N}(1+\alpha_1+\alpha_2)^2}{\Delta} \right], i \neq i'$$

$$\text{Cov}(\hat{\beta}_0, \hat{\beta}_{ii}) = 0$$

The estimated response at the point  $\mathbf{x}_0$  is  $\hat{y}_0 = \mathbf{x}_0' \hat{\boldsymbol{\beta}} = \hat{\beta}_0 + \sum_{i=1}^2 \hat{\beta}_i x_{i0} + \sum_{i=1}^2 \hat{\beta}_{ii} x_{i0}^2$  with its variance

$$V(\hat{y}_0) = \mathbf{x}_0' V(\hat{\boldsymbol{\beta}}) \mathbf{x}_0 = \sigma^2 \mathbf{x}_0' (\mathbf{Z}' \mathbf{Z})^{-1} \mathbf{x}_0.$$

Thus,

$$\begin{aligned} V(\hat{y}_0) &= V(\hat{\beta}_0) + V(\hat{\beta}_i) \sum_{i=1}^v x_{i0}^2 + V(\hat{\beta}_{ii}) \sum_{i=1}^v x_{i0}^4 \\ &+ 2 \text{Cov}(\hat{\beta}_0, \hat{\beta}_{ii}) \sum_{i=1}^v x_{i0}^2 + 2 \text{cov}(\hat{\beta}_{ii}, \hat{\beta}_{i'i'}) \sum_{i=1}^{v-1} \sum_{i'=i+1}^v x_{i0}^2 x_{i'0}^2 \end{aligned}$$

Therefore,

$$\begin{aligned} V(\hat{y}_0) \sigma^{-2} &= \frac{1}{N(1 + \alpha_1 + \alpha_2)^2} [1 + 2\delta(1 + \alpha_1 + \alpha_2)^2 \xi] \\ &+ \left\{ \frac{1}{[(1 + \alpha_1^2 + \alpha_2^2)\delta + A]} - 2\xi \right\} \sum_{i=1}^v x_{i0}^2 \\ &+ \frac{(1 + \alpha_1^2 + \alpha_2^2)L(C + 1) + B + D - 2(1 + \alpha_1^2 + \alpha_2^2) \frac{\delta^2}{N}}{\Delta} \sum_{i=1}^v x_{i0}^4 \\ &- 2 \frac{[(1 + \alpha_1^2 + \alpha_2^2)L + D - \frac{\delta^2}{N}(1 + \alpha_1 + \alpha_2)^2]}{\Delta} \sum_{i=1}^{v-1} \sum_{i'=i+1}^v x_{i0}^2 x_{i'0}^2 \end{aligned}$$

For  $v$  factors,

$$\mathbf{Z}' \mathbf{Z} = \left[ \begin{array}{cc|c} N(1 + \alpha_1 + \alpha_2)^2 & \mathbf{0}'_{1 \times v} & (1 + \alpha_1 + \alpha_2)^2 \delta \mathbf{1}'_{1 \times v} \\ \mathbf{0}'_{v \times 1} & [(1 + \alpha_1^2 + \alpha_2^2)\delta + A] \mathbf{I}_v & \mathbf{0}_{v \times v} \\ (1 + \alpha_1 + \alpha_2)^2 \delta \mathbf{1}_{v \times 1} & \mathbf{0}_{v \times v} & \mathbf{H}_{v \times v} \end{array} \right]$$

with

$$(\mathbf{Z}' \mathbf{Z})^{-1} = \left[ \begin{array}{cc|c} \frac{1}{N(1 + \alpha_1 + \alpha_2)^2} + 2 \frac{\delta}{N} \xi & \mathbf{0}'_{1 \times v} & -\xi \mathbf{1}'_{1 \times v} \\ \mathbf{0}_{v \times 1} & \frac{1}{[(1 + \alpha_1^2 + \alpha_2^2)\delta + A]} \mathbf{I}_v & \mathbf{0}_{v \times v} \\ -\xi \mathbf{1}_{v \times 1} & \mathbf{0}_{v \times v} & \boldsymbol{\Psi} \end{array} \right],$$

where,

$$\xi = \frac{\delta}{N}$$

$$\left[ \frac{[(1 + \alpha_1^2 + \alpha_2^2)L(C - 1) + B - D] + (v - 1) \left[ (1 + \alpha_1^2 + \alpha_2^2)L + D - \frac{\delta^2}{N}(1 + \alpha_1 + \alpha_2)^2 \right]}{\Delta} \right],$$

$$\Psi = \left[ \frac{(1 + \alpha_1^2 + \alpha_2^2)L(C + v - 1) + B + (v - 1)D - v \frac{\delta^2}{N}(1 + \alpha_1 + \alpha_2)^2}{\Delta} \right] \mathbf{I}_v$$

$$+ \left[ -\frac{(1 + \alpha_1^2 + \alpha_2^2)L + D - \frac{\delta^2}{N}(1 + \alpha_1 + \alpha_2)^2}{\Delta} \right] \mathbf{1}\mathbf{1}',$$

and

$$\Delta = [(1 + \alpha_1^2 + \alpha_2^2)L(C - 1) + B - D]$$

$$\left\{ \begin{array}{l} [(1 + \alpha_1^2 + \alpha_2^2)L(C - 1) + B - D] + \\ v \left[ (1 + \alpha_1^2 + \alpha_2^2)L + D - \frac{\delta^2}{N}(1 + \alpha_1 + \alpha_2)^2 \right] \end{array} \right\}$$

Thus, expression for variances/covariances of the estimates are

$$V(\hat{\beta}_0) = \frac{\sigma^2}{N(1 + \alpha_1 + \alpha_2)^2} [1 + v\delta(1 + \alpha_1 + \alpha_2)^2\xi]$$

$$V(\hat{\beta}_i) = \frac{\sigma^2}{[(1 + \alpha_1^2 + \alpha_2^2)\delta + A]} \text{ for } i = 1, 2, \dots, v$$

$$V(\hat{\beta}_{ii}) = \sigma^2$$

$$\left[ \frac{(1 + \alpha_1^2 + \alpha_2^2)L(C + v - 1) + B + (v - 1)D - v \frac{\delta^2}{N}(1 + \alpha_1 + \alpha_2)^2}{\Delta} \right]$$

$$\text{Cov}(\hat{\beta}_0, \hat{\beta}_{ii}) = -\sigma^2\xi$$

$$\text{Cov}(\hat{\beta}_{ii}, \hat{\beta}_{i'i'}) = \sigma^2 \left[ -\frac{(1 + \alpha_1^2 + \alpha_2^2)L + D - \frac{\delta^2}{N}(1 + \alpha_1 + \alpha_2)^2}{\Delta} \right]$$

$$\text{Cov}(\hat{\beta}_0, \hat{\beta}_i) = 0 \quad (3.5)$$

The estimated response at the point  $\mathbf{x}_0$  is  $\hat{y}_0 = \mathbf{x}_0'\hat{\beta} = \hat{\beta}_0 + \sum_{i=1}^v \hat{\beta}_i x_{i0} +$

$\sum_{i=1}^v \hat{\beta}_{ii} x_{i0}^2$  with its variance

$$V(\hat{y}_0) = V(\hat{\beta}_0) + V(\hat{\beta}_i) \sum_{i=1}^v x_{i0}^2 + V(\hat{\beta}_{ii}) \sum_{i=1}^v x_{i0}^4$$

$$+ 2 \text{Cov}(\hat{\beta}_0, \hat{\beta}_{ii}) \sum_{i=1}^v x_{i0}^2 + 2 \text{cov}(\hat{\beta}_{ii}, \hat{\beta}_{i'i'}) \sum_{i=1}^{v-1} \sum_{i'=i+1}^v x_{i0}^2 x_{i'0}^2$$

Using (3.5), we get

$$\begin{aligned}
 V(\hat{y}_0)\sigma^{-2} &= \frac{1}{N(1 + \alpha_1 + \alpha_2)^2} [1 + 2\delta(1 + \alpha_1 + \alpha_2)^2\xi] \\
 &+ \left\{ \frac{1}{[(1 + \alpha_1^2 + \alpha_2^2)\delta + A]} - 2\xi \right\} \sum_{i=1}^v x_{i0}^2 + \\
 &\frac{(1 + \alpha_1^2 + \alpha_2^2)L(C + v - 1) + B + (v - 1)D - v\frac{\delta^2}{N}(1 + \alpha_1 + \alpha_2)^2}{\Delta} \sum_{i=1}^v x_{i0}^4 \\
 &- 2 \frac{[(1 + \alpha_1^2 + \alpha_2^2)L + D - \frac{\delta^2}{N}(1 + \alpha_1 + \alpha_2)^2]}{\Delta} \sum_{i=1}^{v-1} \sum_{i'=i+1}^v x_{i0}^2 x_{i'0}^2
 \end{aligned}$$

A design under this situation is said to be rotatable if this variance is same for all points  $\mathbf{x}$  which are equidistant from the design centre and the designs satisfying this property are called as Second Order Rotatable Designs with Differential Neighbour Effects (SORDDNE).

**Remark :** For  $\alpha_1 = \alpha_2 = \alpha$ , the above expression reduces to Sarika *et al.* (2009).

### 3.1 Method of Constructing SORDDNE

Considering the method given in section 2.1, construct a  $3^v$  full factorial with levels  $(-1, 0, 1)$  giving a rectangle  $R$  of  $3^v$  rows and  $v$  columns with entries  $-1, 0$  and  $1$ . Circular rotation of the columns of  $R$ ,  $(v - 1)$  times, yields  $(v - 1)$  sets each consisting of  $3^v$  rows and  $v$  columns. By appending these sets below  $R$  one after another, we obtain a rectangular array of  $v \times 3^v$  rows and  $v$  columns. Appending another  $(v + 1)$  columns (a column of unity and  $v$  columns of square terms), a SORDDNE in  $v \times 3^v$  points is obtained by adding two extra points of border units such that each end of the array has a point of the other end.

**Example 3.1** For  $v = 2$  ( $X_1$  and  $X_2$ ), the design matrix,  $\mathbf{X}$  in 18 points with two border points is as follows:

$$\mathbf{X}_{20-5} = \begin{bmatrix} 1 & -1 & -1 & 1 & 1 \\ 1 & 1 & 1 & 1 & 1 \\ 1 & 0 & 1 & 0 & 1 \\ 1 & -1 & 1 & 1 & 1 \\ 1 & 1 & 0 & 1 & 1 \\ 1 & 0 & 0 & 0 & 0 \\ 1 & -1 & 0 & 1 & 0 \\ 1 & 1 & -1 & 1 & 1 \\ 1 & 0 & -1 & 0 & 1 \\ 1 & -1 & -1 & 1 & 1 \\ 1 & 1 & 1 & 1 & 1 \\ 1 & 1 & 0 & 1 & 0 \\ 1 & 1 & -1 & 1 & 1 \\ 1 & 0 & 1 & 0 & 1 \\ 1 & 0 & 0 & 0 & 0 \\ 1 & 0 & -1 & 0 & 1 \\ 1 & -1 & 1 & 1 & 1 \\ 1 & -1 & 0 & 1 & 0 \\ 1 & -1 & -1 & 1 & 1 \\ 1 & 1 & 1 & 1 & 1 \end{bmatrix}$$

For  $\alpha_1 = 0.6$  and  $\alpha_2 = 0.4$

$$\mathbf{Z}'\mathbf{Z} = \begin{bmatrix} 72 & 0 & 0 & 48 & 48 \\ 0 & 16.8 & 0 & 0 & 0 \\ 0 & 0 & 16.8 & 0 & 0 \\ 48 & 0 & 0 & 37.6 & 32 \\ 48 & 0 & 0 & 32 & 37.6 \end{bmatrix}$$

Hence,

$$V(\hat{\beta}_0) = 0.172\sigma^2, V(\hat{\beta}_i) = 0.059\sigma^2, V(\hat{\beta}_{ii}) = 0.178\sigma^2,$$

$$\text{Cov}(\hat{\beta}_0, \hat{\beta}_{ii}) = -0.1090 \text{ and } V(\hat{y}_0) = 0.1726\sigma^2$$

Here, the variance of the estimated response is the same for all the points in the design and hence the design is rotatable.

#### 4. CONCLUSIONS

The problem of neighbour effects is common in experiments conducted in the field. In response surface analysis, the presence of neighbour effect cannot be ignored as it may affect the precision of the parameter estimates of the model and hence of the estimated response. The methodology developed here may be useful to tackle the problem of neighbour effects and to get

precise estimates of parameters. The technique has been illustrated through a simulated data set. Designs have been obtained for the experimental situations where neighbour effect is suspected. The design obtained here is considerably larger as compared to the designs used for fitting response surface without the neighbouring contamination, but this structure is needed to ensure proper estimation when neighbour effect is suspected.

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